



# Effects of Heat Treatment on Magnetic Properties of NdFeB Based Permanent Magnet Alloys

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## Abstract

In this study, the effect of flash annealing heat treatment applied at 680 °C for 5 minutes on the magnetic properties of NdFeB-based permanent magnet alloys produced by melt spinning method, which is one of the fast solidification methods, was investigated by using a very fast heating and cooling rate of 300 K/s. The obtained results showed that there was a remarkable improvement in the magnetic properties of the alloys with the applied heat treatment. Mainly, the hard magnetic properties were optimized by enhancing magnetic remanence from 21.64 emu/g to 55.76 emu/g, magnetic coercivity from 1184.15 Oe to 9146.30 Oe, and maximum energy product from 4.06 kJ/m<sup>3</sup> to 62.02 kJ/m<sup>3</sup> respectively.

**Keywords:** NdFeB alloys, Melt spinning, Heat treatment, Magnetic properties.

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## 1. Introduction

The development of NdFeB-based permanent magnets occurred in the early 1980s [1]. This type of permanent magnets, thanks to their superior magnetic properties [2], are becoming increasingly indispensable for societies in parallel with the developing technology day by day [3]. These magnetic properties are high remanence ( $B_r$ ), high coercivity ( $H_c$ ) [4], and these properties also enable them to have a high maximum energy product,  $(BH)_{max}$  [1, 5]. Their superior magnetic properties; make it possible for them to be widely used in many fields such as hybrid electric vehicles [9] and energy storage systems [10], as well as in fields such as electronics [6], aviation [7], and medical [8]. In the production of NdFeB-based permanent magnets, methods such as rapid solidification (for example, melt spinning), atomization, HDDR process, mechanical alloying, severe plastic deformation, powder metallurgy are used [11]. The development of the application areas of NdFeB-based permanent magnets necessitates the optimization of their magnetic properties. For example, if they are used in hybrid engines, they should have a very high coercivity (approximately 2500 kA/m) and be able to maintain magnetic stability up to 150 °C [8]. It can be said that this situation increases the need for NdFeB magnets with high  $(BH)_{max}$  and high  $H_c$  properties. Among the existing production methods, melt spinning method is a type of rapid solidification method using very high cooling rates (as high as  $10^9$  K/s), it provides amorphous and/or nanocrystalline structures [12,13] and thus superior magnetic properties such as high  $H_c$  and  $(BH)_{max}$  unique to permanent magnets [1].

As is known, the modification of the magnetic properties of NdFeB-based magnets can be achieved with any applied heat treatment [14]. In this respect, the main purpose of our current study is to examine the effect of flash annealing heat treatment applied by rapidly heating NdFeB based alloys produced by melt spinning method to 680 °C temperature and cooling them rapidly after applying heat treatment for 5 minutes.

## 2. Material and Method

In order to produce NdFeB-based ribbon alloys, first of all, ingot alloys were produced under a high vacuum (approximately  $10^{-6}$  mbar) and in the argon atmosphere (approximately 550 mbar partial pressure) with the help of a vacuum induction melting (VIM) furnace. Nominal chemical composition of the alloys was adjusted to 36% Nd, 62% Fe and 2% B by weight. For each ingot alloy, the melting process was repeated 5 times to ensure maximum homogeneity. The weight of each ingot alloy produced were 260 g. For producing NdFeB based alloys in the ribbon form in melt spinning process, by means of a nozzle with a cross section of  $1 \times 8$  mm<sup>2</sup>, the liquid metal re-melted under vacuum was ejected onto a copper wheel rotating at a speed of approximately 35 m/s. While the argon partial pressure used to eject the liquid metal onto the copper wheel was 250 mbar, the distance between the wheel and the nozzle was adjusted to 0.5 mm, and thus NdFeB alloys in the form of ribbon with a homogeneous thickness of 8 µm and a width of 25 mm were produced. X-ray diffraction (XRD) analysis (with Cu-K $\alpha$  radiation) was performed to detect the crystalline and amorphous regions in the alloys. Vibrating sample magnetometer (VSM) analysis was performed to determine the magnetic properties of each alloy. In order to examine the effect of heat treatment on crystallization and magnetic properties, flash annealing heat treatment was applied at very rapid heating and

cooling rates of 300 K/s for 5 minutes, at 680 °C, respectively. The description of each alloy produced within the scope of this study is summarized in Table 1.

Table 1. Description of melt spun NdFeB based alloys that are not heat treated and heat treated at 680 °C for 5 minutes

Melt spun alloys	Description
N0	Melt spun, non-heat treated
N680-5	Melt spun, heat treated at 680 °C for 5 minutes

## 3. Results and Discussion

In Fig. 1, the XRD patterns of the NdFeB based alloys produced by the melt spinning method are shown in the non-heat treated and heat treated state at 680 °C for 5 minutes. Accordingly, it can be clearly seen that each melt spun NdFeB alloy exhibits an amorphous structure with traces of crystalline structure. The rapid cooling used in the melt spinning method is the main reason for obtaining the amorphous structure [15]. The XRD pattern of the non-heat treated alloy is seen with the crystalline peak of the hard magnetic Nd<sub>2</sub>Fe<sub>14</sub>B phase at an angle of about  $2\theta=30^\circ$  and the peak of the soft magnetic  $\alpha$ -Fe phase at an angle of  $2\theta=45^\circ$ . With the applied flash annealing heat treatment, an increase in the intensity of the peaks belonging to the hard and soft magnetic phases was observed. In other words, a transformation from amorphous structure to crystal structure has taken place here [16]. A certain temperature and time are required for the atoms in the material to pass from the amorphous structure to the crystalline order [17]. At high temperatures and/or long periods of time, atomic mobility increases, so crystallization occurs more [18].

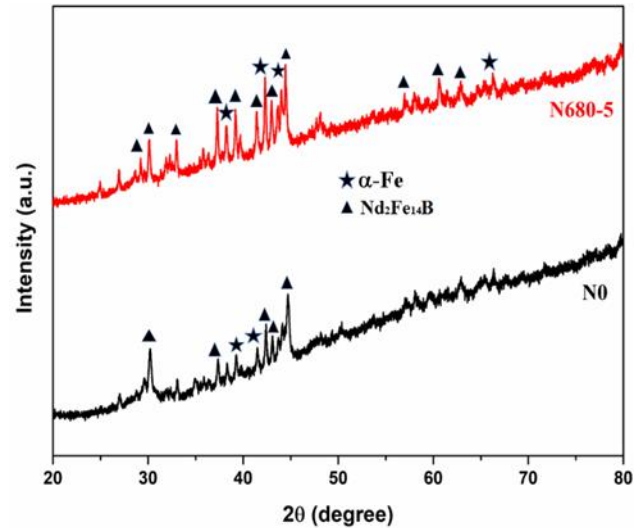


Fig 1. XRD patterns of melt spun NdFeB based alloys in the non-heat treated (N0) and heat treated condition (N680-5) at 680 °C for 5 min.

Fig. 2 shows the results of differential scanning calorimetry (DSC) analyzes applied to determine the Curie temperatures of melt spun NdFeB based alloys at non-heat treated and heat treated conditions at 680 °C for 5 min. According to the obtained DSC analysis results, the Curie temperatures ( $T_c$ ) of melt spun alloys are 302 °C for the non-heat treated alloy and 310 °C for heat treated at 680 °C for 5 min. respectively. These results are consistent with those of Haiyang et al.'s study. [19] and a slight increase in  $T_c$  temperature occurred with the applied flash annealing heat treatment. Whereas, recrystallization temperatures

are 380 °C for the non-heat treated alloy and 388 °C for the heat treated alloy at 680 °C for 5 min.

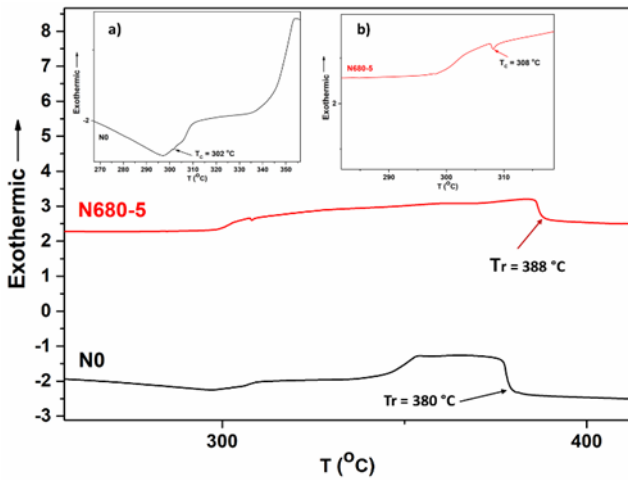


Fig 2. DSC curves of melt spun NdFeB based alloys in the non-heat treated (N0) and heat treated (N680-5) condition at 680 °C for 5 minutes.

In Fig. 3 and 4, the demagnetization curves and second quadrant of the demagnetization curves of melt-spun NdFeB based alloys and are shown in the non-heat treated and heat treated condition at 680 for 5 minutes, respectively. As can be seen, in the non-heat treated alloy, magnetic coercivity ( $H_c$ ), 1184.15 Oe, maximum energy product ( $(BH)_{max}$ ), 4.06 kJ/m<sup>3</sup>, magnetic remanance ( $B_r$ ), 21.64 emu/g and saturation magnetization ( $B_s$ ), 93.50 emu/g. With the heat treatment applied for 680 °C and 5 minutes, an increase was observed in  $H_c$ ,  $(BH)_{max}$ ,  $B_r$  and  $B_s$  properties, and an improvement was observed towards 9146.30 Oe, 62.02 kJ/m<sup>3</sup>, 55.76 emu/g and 104.65 emu/g, respectively. This increase in magnetic properties can be explained by the emergence of more nanocrystalline  $\alpha$ -Fe soft magnetic phase and Nd<sub>2</sub>Fe<sub>14</sub>B hard magnetic phases with the effect of applied flash annealing heat treatment and the dominance of hard magnetic Nd<sub>2</sub>Fe<sub>14</sub>B phase [18]. According to the exchange coupling mechanism that occurs between the hard and soft magnetic phases, the magnetic moment of the soft magnetic phase rotates along the boundaries of the hard magnetic phase, which provides an improvement in the permanent magnetic properties [20]. In Table 2, the magnetic properties of melt spun NdFeB based alloys, at non-heat treated and heat treated condition at 680 °C for 5 minutes, are summarized.

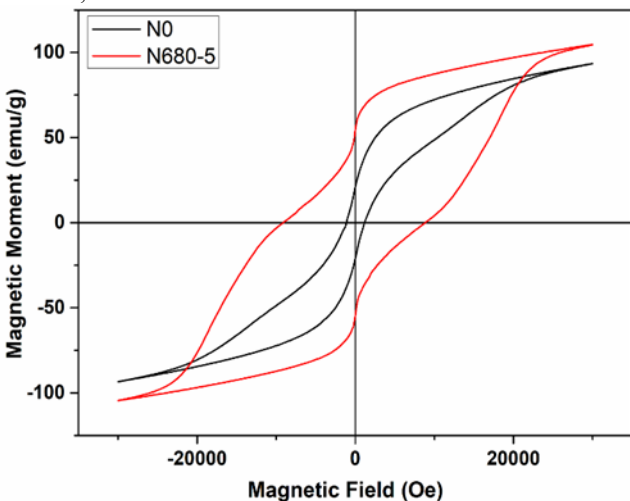


Fig 3. VSM curves of melt spun NdFeB based alloys in non-heat treated (N0) and heat treated (N680-5) condition at 680 °C for 5 minutes.

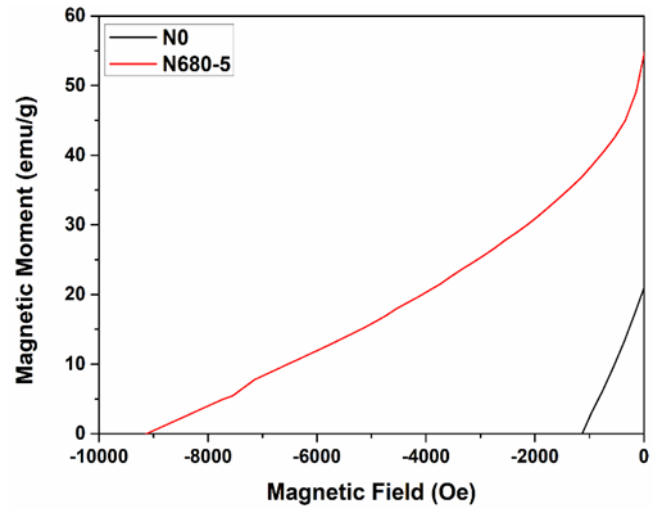


Fig 4. Second quadrant parts of VSM curves of melt spun NdFeB based alloys in the non-heat treated (N0) and heat treated (N680-5) condition at 680 °C for 5 minutes.

Table 1. Summary of the magnetic properties of melt spun NdFeB based alloys in the non-heat treated (N0) and heat treated (N680-5) condition at 680 °C for 5 min.

Melt spun alloy	$B_s$ (emu/g)	$B_r$ (emu/g)	$H_c$ (Oe)	$(BH)_{max}$ (kJ/m <sup>3</sup> )
N0	93.50	21.64	1184.15	4.06
N680-5	104.65	55.76	9146.30	62.02

## 4. Conclusions and Recommendations

Within the scope of our study, the effect of flash annealing heat treatment applied at 680 °C and for 5 minutes using very rapid heating and cooling rates on the magnetic properties of NdFeB based permanent magnet alloys produced using the melt spinning method by rapid solidification is discussed. The XRD pattern of the non-heat treated alloy reveals the coexistence of amorphous and nanocrystalline  $\alpha$ -Fe soft magnetic and Nd<sub>2</sub>Fe<sub>14</sub>B hard magnetic phases. Optimization was achieved in the hard magnetic properties, with the emergence of more soft and hard magnetic phases with the crystallization caused by the effect of the applied heat treatment, and the improvement in magnetic properties such as  $H_c$ ,  $B_r$  and  $(BH)_{max}$ , especially with the dominance of the hard magnetic Nd<sub>2</sub>Fe<sub>14</sub>B phase.

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